RD® pile wall

DESIGN AND INSTALLATION MANUAL

This RD® pile wall Design and Installation Manual deals with retaining wall solutions using drilled SSAB’s RD piles. The design methods shown here are based on Eurocode standards.

The manual presents the basics of RD pile wall design and installation, recommendations for choosing the most suitable pile size and interlock type, instructions for handling and installation, as well as instructions for quality control, measurements and documentation.

The manual also includes pre-calculated tables and implementation examples to facilitate the design and execution of an RD pile wall solution.

Applications:
- permanent retaining walls
- structures under combined lateral and vertical loads
- bridge abutments
- basement parking facilities
- watertight retaining walls
- retaining walls and excavations extending to bedrock

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FOREWORD

SSAB is one of the leading suppliers of steel foundation structures in Europe. Our domestic market includes the Nordic countries and the Baltic Sea region, but owing to our effective logistics we are also able to deliver solutions for demanding projects elsewhere in Europe.

SSAB is your skilled partner. The solutions we offer are economically competitive and technically advanced. They are based on comprehensive expertise and responsible operating procedures. For us, partnership with the customer means not only commitment to high reliability and promptness of delivery, but also to consulting in the design and implementation stage where required.

The RD® pile wall is SSAB’s retaining wall solution based on RD® piles. An RD pile wall is specially designed for challenging conditions, for instance, for faster implementation of retaining walls and other foundation structures. You can always find the correct pile size and steel grade from SSAB’s extensive RD pile range to allow you to build a retaining wall or foundation structure with the best overall economy for all soil conditions and loading situations. By selecting SSAB’s delivery package, enables you to also take advantage of all other steel components, systems and overall solutions for your foundation engineering project with ease from one supplier.
Vertically loaded structures

If the piles are extended to the bedrock, the vertical load-bearing capacity of the RD pile wall is very high. Thus the structure can act as a horizontally loaded wall subject to earth pressure and a foundation structure able to bear high vertical loads at the same time.

1.1 Application examples

Building with a basement

An RD pile wall may be used to good advantage in buildings with one or more basement storeys. In such projects, the RD pile wall serves as a permanent joint structure for vertical and horizontal loads. The solution is cost effective because no separate retaining wall structures are needed. An RD pile wall can be surface treated and allowed to remain an exposed wall structure, for example, in parking facilities in a basement without internal cladding. Figure 1 shows an example of an RD pile wall in a building with a basement.

Building with a column frame

An RD pile wall may consist of piles of variable length. Some of the piles of the RD pile wall can be extended to the bedrock to ensure horizontal support for the lower end of the wall structure, and to act as foundation piles that transport column loads. Figure 2 shows an example of an RD pile wall in a building with a column frame.

An RD pile wall may also be built as a so-called Combi wall, with sheet piles installed between the RD piles fitted with interlocks by driving them by driving or vibration after installation of the pipe piles.

Figure 1. RD pile wall in a building with a basement.

Figure 2. RD pile wall in a building with a column frame.
**Temporary retaining wall during construction**

An RD pile wall is an effective solution for temporary retaining wall structures during construction in conditions where the soil contains strata that are difficult to penetrate, high water tightness is required of the retaining wall, there is a need to minimize the number of support levels, or the retaining wall must be extended into the bedrock. Installation of RD pile walls usually causes less vibration when penetrating compact soil layers than the installation of sheet pile walls. This makes the RD pile wall very suitable for installation close to vibration-sensitive structures. Figure 3 shows an example of the RD pile wall as a temporary retaining wall during construction.

**Retaining walls of various shapes**

RD pile walls may be used for building wall assemblies of different geometric shapes. For instance, the walls can be circular or make angles of various degrees. If necessary, an RD pile wall can consist of a combination of different pile sizes. This enables the wall structure to be optimized according to actual loads. Figure 4 shows an example of an RD pile wall used as a retaining wall of different shape.

**Excavations and structures extending into the bedrock**

If the support of the bottom of the retaining wall, the excavation level or water tightness requires the retaining wall to be extended securely into the bedrock or several meters into moraine containing stones and boulders, sheet pile walls cannot be used without special measures such as pre-drilling, blasting, etc. A temporary or permanent RD pile wall can be drilled to the desired level in the bedrock. The rock bounded by the wall may be excavated up to the wall, whereby construction work requires less space because there is no need for a “rock shelf” on which the retaining wall rests. Figure 5 shows an example of an RD pile wall as an excavation wall extending into the bedrock.

**Bridge abutments**

An RD pile wall can be used as a bridge abutment (Figure 6). With the RD pile wall, the vertical and lateral loads of the bridge and the horizontal loads of the embankment can be transferred reliably to the bedrock and soil. Use of an RD pile wall as an abutment allows the bridge deck to be built before excavation. This can be combined, for instance, with a method to move the deck to minimize traffic disruption during construction.

**Intermediate bridge supports**

RD pile walls can be used for intermediate bridge supports subject to heavy horizontal loads, such as impact loads, under difficult soil and environmental conditions. A closed frame extending into the bedrock can be built with an RD pile wall under an intermediate column and the soil removed from top part for concreting (Figure 7). The structure does not require separate temporary retaining structures during construction and the foundations can be implemented in cramped conditions.
Harbor wharves

RD pile walls can be used for building wharves in challenging soil conditions. If necessary, the piles can be protected against corrosion, for example, by painting as shown in Figure 8. An RD pile wall can be built of SSAB’s high strength piles of grade S550J2H steel. A high-strength steel grade provides the structure with high bending resistance in relation to material consumption.

Wind turbine foundations

RD pile walls can be used to build integral foundation wall structures for off-shore facilities. The RD pile wall foundation is particularly suitable for conditions where the installation of large mono-piles requires special measures or, for example, a caisson foundation would require massive soil replacement. An RD pile wall foundation allows wind turbines to be built also in shallow water in all soil conditions as shown in Figure 9.

Trough structures

RD pile walls can be used to implement watertight trough structures which allow, for example, a road to be built below groundwater level without lowering the surrounding groundwater table. If RD piles are extended watertightly into the bedrock (Figure 10), there is no need to anchor the foundation slab of the trough structure against buoyancy. In temporary retaining walls during construction, pipe piles can be used as temporary pump wells to keep excavation dry.
2 NORMATIVE REFERENCES

These instructions incorporate references from other publications. These references are cited at the appropriate places in the text and the publications are listed hereafter.


EN 1090-2:2018 Execution of steel structures and aluminium structures. Part 2: Technical requirements for steel structures


EN 10020:2000 Definitions and classification of grades of steel

EN 10219-1:2006 Cold formed structural welded hollow sections of non-alloy and fine grain steels – Part 1: Technical delivery requirements

EN 10219-2:2006 Cold formed welded structural hollow sections of non-alloy and fine grain steels – Part 2: Tolerances, dimensions and sectional properties


EN 16228-2:2014 Drilling and foundation equipment. Safety. Part 2: Mobile drill rigs for civil and geotechnical engineering, quarrying and mining

EN 16228-7:2014 Drilling and foundation equipment. Safety. Part 7: Interchangeable auxiliary equipment
3 DEFINITIONS

**Anchorage**
Anchoring system for a retaining wall, for example anchor plates or anchor walls including the connecting rods (tie rods), screw anchors, ground and rock anchors, driven ground anchors, anchoring piles and anchors with grouted or expanded bodies.

**Auxiliary structures**
All structures necessary for the proper and safe execution of pile wall and sheet piling work.

**Bracing**
System of walings and struts to support the structure.

**Caterpillar track level**
Elevation of bottom of caterpillar tracks of piling equipment.

**Combined wall**
Retaining wall composed of primary and secondary elements. The primary elements can be steel tubes, beams or box piles. The secondary elements are normally U or Z-shaped steel sheet piles.

**Guide frame**
Frame consisting of one or more stiff guide beams, normally of steel or wood, to position and maintain the alignment of sheet piles during pitching and driving.

**Interlock**
Steel profile attached to pile pipes which connects and locks adjacent pile pipes or sheet piles together.

**Pile wall**
Screen of pile pipes which forms a continuous wall. Continuity is provided by interlocks attached to pile pipes.

**Pile wall structure**
Structure, consisting of pile pipes, sheet piles, soil and rock anchorages, bracings and walings, which retains ground and water.

**Sheet pile wall**
Screen of sheet piles which forms a continuous wall. For steel sheet piles continuity is provided by interlocking of the joints, fitting of longitudinal grooves or by means of special connectors and for timber sheet piles, by tongue and groove.

**Site inspection**
Inspection of the construction site and its surroundings.

**Site investigation**
Geotechnical investigations on and near the construction site.

**Strut**
Long compression member, usually of steel, wood or reinforced concrete, for the support of the pile walls and normally connected to the walings.

**Waling**
Horizontal beam, usually of steel or reinforced concrete, fixed to the pile wall and connected to the anchorage or struts, in order to distribute the applied anchor or strut forces equally over the pile wall.

4 INFORMATION NEEDED TO INSTALL RD PILE WALLS

4.1 General

The following information shall be made available before commencing installation of the RD pile wall structure:

- location maps of the construction site, including access roads and possible obstacles;
- level and position of fixed reference points at or near the construction site;
- access restrictions concerning equipment and materials;
- location of all services such as electricity, telephone, water and gas supply pipes, and sewers;
- geotechnical data of the construction site;
- composition and stratification of the ground and its variation across the site;
- strength and deformation properties of the soil and rock layers;
- possible presence of stones and boulders in the ground;
- possibility of cohesive soils adhering to the piles when extracted (see 8.11);
- hydrogeological data of the area in which the construction site will be situated;
- specifications, including full details such as pile size, steel grade, protection and preservation systems and also whether any interlock fixings are required to ensure transmission of the longitudinal shear forces;
- presence of sensitive buildings and/or installations in the vicinity of the construction site;
- noise and vibration restrictions;
- drilling method and drilling assistance restrictions;
- restrictions regarding the permeability of the retaining wall for water or other fluids;
- various stages of building the wall structure required by the design;
- in the case of waterfront structures; the water levels and their fluctuations (amplitude, frequency and the cause of the fluctuations, e.g. discharge of a barrage, tide, etc.);
- data regarding possible soil contamination;
- list of any identified specific items to be investigated (see 4.2).
4.2 Specific

The following specific information shall be made available work commences;
- all specific design information which is important to building an RD pile wall;
- restrictions related to the presence, at or near the site, of ground anchors, cathodic protection devices and similar;
- history of the building site: presence of foundation remnants or other artificial elements in the ground.

Information about the following should be made available before work commences:
- special aspects particular to the project, such as corrosion and abrasion problems;
- comparable experience from work in the neighborhood or from similar work carried out under similar conditions;
- condition of nearby buildings, structures or installations and the nature and depth of their foundation;
- data about adverse weather conditions, for example, wind conditions and frequency;
- severe frost action in the ground, where this can lead to overstressing of an wall.

5 SITE INVESTIGATIONS

The content and scope of the geotechnical site investigation program should be designed to take into account the demands of ground conditions, taking into consideration the environment and trench structures. The geotechnical investigation program must include geotechnical surveys taking into account excavation work risk management, work planning and quality control. Test points should be positioned to correspond as closely as possible to the final location of the excavation structure. Target levels of retaining walls must be determined from research points located on the final wall line.

5.1 Rock and soil investigations

Geotechnical investigations must provide sufficient data on the ground and groundwater conditions at and around the excavation site for a proper description of the essential ground properties and a reliable assessment of the characteristic values of the ground parameters to be used in determining earth pressures on the retaining wall. Geotechnical investigations determine the target level of the piles, which enables the order of cut-to-size piles and avoids extra loss of material. If the RD pile wall is extended to the bedrock, the variations in elevation and the quality of the bedrock surface must be determined by percussion drilling.

Basic scope of geotechnical investigations should be at least 1 test point / 10 meters at the wall line. If the RD pile wall is extended to the bedrock, percussion drilling must be used, and boreholes must penetrate at least 3 meters into the bedrock. In challenging projects and soil conditions, drill point frequency should be 1 test point / 3...5 meters.

Extensive geotechnical investigations combined with factory deliveries with specific pile lengths creates the basis for both the structural and financial success of the project without need of changes during installation work.

Any investigations must comply with Section 3 of EN 1997-1.

6 MATERIALS AND ACCESSORIES

6.1 Pile pipes

RD pile walls can be made out of different pile sizes ranging from pile RD220 up to RD1200. The piles are delivered in exact predefined lengths and, when needed, with welding bevels. Table 1 shows the pile sizes used in RD pile walls.

<table>
<thead>
<tr>
<th>Pile</th>
<th>Diameter [mm]</th>
<th>Weight [kg/m]</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>10</td>
<td>12.5</td>
</tr>
<tr>
<td>RD220</td>
<td>219.1</td>
<td>51.6</td>
</tr>
<tr>
<td>RD270</td>
<td>273.0</td>
<td>64.9</td>
</tr>
<tr>
<td>RD320</td>
<td>323.9</td>
<td>77.4</td>
</tr>
<tr>
<td>RD400</td>
<td>406.4</td>
<td>97.8</td>
</tr>
<tr>
<td>RD500</td>
<td>508.0</td>
<td>122.8</td>
</tr>
<tr>
<td>RD600</td>
<td>610.0</td>
<td>148.0</td>
</tr>
<tr>
<td>RD700</td>
<td>711.0</td>
<td>172.9</td>
</tr>
<tr>
<td>RD800</td>
<td>813.0</td>
<td>198.0</td>
</tr>
<tr>
<td>RD900</td>
<td>914.0</td>
<td>222.9</td>
</tr>
<tr>
<td>RD1000</td>
<td>1016.0</td>
<td>248.1</td>
</tr>
<tr>
<td>RD1200</td>
<td>1220.0</td>
<td>298.4</td>
</tr>
</tbody>
</table>

Table 1. Pile sizes used in RD pile walls.
Steel grades of piles

SSAB steel grades S440J2H, S460MH and S550J2H, manufactured especially for piling, can be used in RD pile walls. For RD pile walls built with RD270 or larger piles, steel grade S355J2H can also be used. Subject to special order, piles may also be supplied in X grades according to API5L. Steel grade can have a significant effect on the structural resistance of the pile wall. For instance, by choosing high-strength steel grade S550J2H it is possible in many cases to reduce pile diameter or wall thickness. Table 1 shows the steel grades available for different pile sizes. Table 2 shows the chemical composition and mechanical properties of steel grades.

Table 2. Standard steel grades for RD pile wall, subject to special order, the piles may also be delivered in or X grades according to API5L.

<table>
<thead>
<tr>
<th>Steel grade</th>
<th>Carbon equivalent</th>
<th>Chemical composition, max.</th>
<th>Mechanical properties</th>
<th>Impact strength</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>CEV max.</td>
<td>C</td>
<td>Mn</td>
<td>P</td>
</tr>
<tr>
<td>---</td>
<td>---</td>
<td>---</td>
<td>---</td>
<td>---</td>
</tr>
<tr>
<td>S355J2H</td>
<td>0.45</td>
<td>0.22</td>
<td>1.6</td>
<td>0.03</td>
</tr>
<tr>
<td>S440J2H</td>
<td>0.45</td>
<td>0.16</td>
<td>1.6</td>
<td>0.02</td>
</tr>
<tr>
<td>S460MH</td>
<td>0.46</td>
<td>0.16</td>
<td>1.7</td>
<td>0.035</td>
</tr>
<tr>
<td>S550J2H</td>
<td>0.47</td>
<td>0.12</td>
<td>1.9</td>
<td>0.02</td>
</tr>
</tbody>
</table>

* Testing temperature may also be -40 °C. Required impact energy remains the same.

6.2 Interlocks

In RD pile walls, the pile pipes are joined to each other by interlocks. Adjacent piles are always locked together with an interlock pair, where one interlock profile is narrow and the other is wide. Two different interlock types have been developed for RD pile walls: the SSAB RM/RF interlock, Figure 11 and E21 interlock, Figure 12.

Water tightness and tight contact between piles and rock can be achieved with an RM/RF interlock without additional injection pipes. When an RM/RF interlock is used, it is also possible to confirm water tightness with post injection without additional injection pipes. RM/RF interlocks are available from pile size RD220 to pile size RD1200. An E21 interlock is used to attach an RD pile wall to a sheet pile wall.

Figure 11. RM/RF interlocks

Figure 12. E21 interlocks
6.3 Drill bits

RD pile walls are installed by the concentric drilling method using ring bits of a larger diameter than standard bits. The ring bit drills a hole larger than the pile to accommodate the pile interlocks. Table 3 shows the recommended ring bit diameters for different piles and interlocking sections. In soft soil conditions with no stones or friction soil layers in ground, smaller diameter drill bits can also be used.

There are two basic types of ring bits: an integrated ring bit (fixed, locked into the casing shoe, Figure 13a) and a solitary ring bit (loose, not locked into the casing shoe, Figure 13b). Both types can be used for RD pile walls. Alternatively, concentric multi-wing pilot bits (Figure 13c) can be used. The wing bits open when drilling starts and are brought back in when drilling ends so that the entire bit, including wings, is lifted up from pile. A casing shoe will not necessarily be part of the load-bearing structure when a multi-wing pilot is used.

When an integrated or solitary ring bit is used, the ring bit and casing shoe will be part of the load-bearing structure of the pile. Since the ring bit and the casing shoe are used as a load-bearing part, they must be able to withstand the stresses exerted on them. The rock shelf may not provide support to the ring bit if it is not filled with concrete or injection grout.

When drilled piles are long or soil conditions are demanding with boulders or stony soils, casing shoe model has an effect on installation reliability. In such cases it has been found out that only surface hardened flat steel ring attached to inner surface of pile pipe is susceptible to deformations and also damaging during installation.

Casing shoes, ring bits and pilots are not part of SSAB’s delivery. Subject to order, casing shoes provided by the customer may be welded to the pile pipes at SSAB’s premises.

Figure 13. Drilling accessories used in RD pile wall construction (Figure: Robit Oyj)
Table 3. Recommended ring bit diameters for different interlocks

<table>
<thead>
<tr>
<th>Pile</th>
<th>Pile diameter [mm]</th>
<th>RM/RF Ring bit diameter [mm]</th>
</tr>
</thead>
<tbody>
<tr>
<td>RD220</td>
<td>219.1</td>
<td>273</td>
</tr>
<tr>
<td>RD270</td>
<td>273.0</td>
<td>327</td>
</tr>
<tr>
<td>RD320</td>
<td>323.9</td>
<td>378</td>
</tr>
<tr>
<td>RD400</td>
<td>406.4</td>
<td>460</td>
</tr>
<tr>
<td>RD500</td>
<td>508.0</td>
<td>562</td>
</tr>
<tr>
<td>RD600</td>
<td>610.0</td>
<td>664</td>
</tr>
<tr>
<td>RD700</td>
<td>711.0</td>
<td>765</td>
</tr>
<tr>
<td>RD800</td>
<td>813.0</td>
<td>867</td>
</tr>
<tr>
<td>RD900</td>
<td>914.0</td>
<td>968</td>
</tr>
<tr>
<td>RD1000</td>
<td>1016.0</td>
<td>1070</td>
</tr>
<tr>
<td>RD1200</td>
<td>1220.0</td>
<td>1274</td>
</tr>
</tbody>
</table>

6.4 Sealants for interlocks

To ensure water tightness of the RD pile wall, the interlocks may be fitted with sealants. There are several sealing materials and manufacturers. Water tightness greatly depends on installation circumstances, ground conditions and the sealing materials used.

The water tightness of RM/RF interlocks with different sealant materials has been tested in laboratory conditions. Table 4 shows the test results for estimated water tightness. The feasibility of the sealant must be estimated separately for each installation site.

Table 4. Water tightness estimate (PU = polyurethane)

<table>
<thead>
<tr>
<th>Sealant material</th>
<th>Water pressure achieved in test [m]</th>
<th>Immediately after installation</th>
<th>1 day after installation</th>
<th>1 month after installation</th>
</tr>
</thead>
<tbody>
<tr>
<td>Plain RM/RF interlock</td>
<td></td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>Bitumen sealant</td>
<td></td>
<td>60*</td>
<td>60*</td>
<td>60*</td>
</tr>
<tr>
<td>PU based sealant after extrusion</td>
<td></td>
<td>0</td>
<td>15*</td>
<td>15*</td>
</tr>
<tr>
<td>PU based sealant after curing</td>
<td></td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>Tar – Grease mix</td>
<td></td>
<td>0</td>
<td>0</td>
<td>0</td>
</tr>
</tbody>
</table>

* The value is the maximum possible water pressure reached with the particular test equipment.

During the water tightness test, also water flow through the RM/RF interlock without a sealant was measured at different water pressure values. Table 5 shows the estimated results.

Table 5. Water flow through an empty RM/RF interlock at different water pressures

<table>
<thead>
<tr>
<th>Water pressure [m]</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
<th>8</th>
<th>9</th>
</tr>
</thead>
<tbody>
<tr>
<td>Empty RM/RF interlock</td>
<td>50</td>
<td>100</td>
<td>150</td>
<td>200</td>
<td>250</td>
<td>300</td>
<td>350</td>
<td>400</td>
<td>450</td>
</tr>
</tbody>
</table>

Sealant material effect on friction

The effect of sealant materials on friction between interlocks has been defined experimentally. Table 6 shows the estimated friction factors to dynamic and static friction. For PU-based sealant material, the friction factors have been defined both instantly after extrusion and after the sealant has cured due to humidity.

Table 6. Effect of different sealant materials on friction between interlocks

<table>
<thead>
<tr>
<th>Sealant material</th>
<th>Experimentally defined friction factor</th>
<th>Static friction</th>
<th>Dynamic friction</th>
</tr>
</thead>
<tbody>
<tr>
<td>Plain RM/RF interlock</td>
<td></td>
<td>0.62</td>
<td>0.50</td>
</tr>
<tr>
<td>Bitumen sealant</td>
<td></td>
<td>0.27</td>
<td>0.23</td>
</tr>
<tr>
<td>PU based sealant after extrusion</td>
<td></td>
<td>0.31</td>
<td>0.27</td>
</tr>
<tr>
<td>PU based sealant after curing</td>
<td></td>
<td>0.26</td>
<td>0.22</td>
</tr>
<tr>
<td>Tar – Grease mix</td>
<td></td>
<td>0.40</td>
<td>0.33</td>
</tr>
</tbody>
</table>

6.5 Other materials and accessories

The structural resistance of the RD pile wall in normal situations as well as under fire can be increased by filling the piles with concrete and by using composite effect. Also reinforcement bars can be used to increase the resistance. Material requirements for concrete and reinforcement bars are the same as when using composite effect on SSAB RR and RD piles generally. Design and installation manual for RR and RD piles has more info on the requirements for concrete and reinforcement bars.

An RD pile wall can be supported externally by soil or rock anchors, or by tension rods attached to anchor plates in the same way as other retaining wall structures. RD pile walls exposed to a high fire risk, i.e. in parking facilities can be protected by separate cladding.
7 DESIGN

7.1 General

In building construction projects, RD pile walls are designed according to Eurocode design standards and additional national regulations. In infrastructure construction, Eurocode design standards are used. An RD pile wall is dimensioned as a conventional retaining wall structure. If an RD pile wall is subjected to significant vertical loads, the design and dimensioning practices of pile foundations are applied in the design.

In some projects, design is also possible using national design instructions approved by other authorities.

Engineering requires adequate input data about the following:
- soil conditions at the wall and a sufficient distance from it
- groundwater conditions
- effect of the environment and the environmentally-imposed conditions such as foundation types of nearby structures
- size and nature of the structure to be supported
- loading and design life of the RD pile wall.

7.2 Selecting pile size

SSAB’s comprehensive pile size and range of steel grades enable cost effective dimensioning of retaining walls. RD piles can be drilled through all possible soil layers and into the solid bedrock if necessary, while location tolerances and curvatures remain relatively small.

If an RD pile wall is designed according to Eurocode design standards as a support structure, the design and dimensioning principles of EN 1997-1, section 9, are observed. If an RD pile wall serves as the foundation of a building, vertical equilibrium must be checked according to the principles of EN 1997-1, section 7. When installed in solid bedrock, the geotechnical resistance of the pile pipe is always higher than the structural resistance of the wall structure.

The structure of an RD pile wall can be designed as a steel structure or as a steel-concrete composite structure. If a pile wall is subject to normal force in addition to bending moment, the pile wall must be dimensioned for the combined stresses. Corrosion of steel piles must be considered in the case of long-term and permanent structures if the piles are not corrosion protected.

Tables 7, 8 and 9 show some of the sectional properties and bending moment resistances of RD pile walls excluding corrosion allowance, or with 1.2 mm or 2.0 mm corrosion allowance reduced from the outer surfaces of the steel piles. Freely downloadable design softwares RRPILECalc and PileWallCalc are available in the SSAB toolbox to calculate cross-section properties or moment resistances for a single steel pipe pile or a pile wall structure. In both programs the pile structure can be a steel, composite structure or a reinforced composite structure. Both programs can be downloaded from www.ssab.com/infra.

The SSAB toolbox also contains Tekla Structures components for easy design and dimensioning of RD pile walls, including allowable design tolerances and assembly lists.

The sizes of tolerances transverse to the wall line are affected mostly by shifts in position during installation. These shifts can be limited by using a sufficiently sturdy guide frame with respect to pile sizes through which the piles are installed.

Both material tolerances and installation tolerances must be considered in design. In design and implementation of wall lines, tolerances must be taken into account especially if the wall incorporates frame columns.

In unrestricted installation space, the smallest recommended pile size is RD270. With smaller pile diameters, the drilling hole oversize required by the interlocks increases significantly in relation to the drill hole diameter of the pile itself. The additional stresses caused for the drill bits and hammers must be taken into account in installation.

In cramped or low installation spaces, such as basements or spaces underneath bridges or fixed roofs, the applicable drilling equipment usually limits the usable pile sizes and element lengths. With small size drilling equipment, the maximum pile size is usually RD220 and the maximum element length 2 meters.

With piles RD600 or larger, the recommended pile wall thickness is 12.5 mm. In easy drilling conditions, for example, with low drilling depth in clay or sandy soils, the applied wall thickness may be smaller.

The stiffness of a pile drilled into the bedrock depends on the applied embedment length, strength of the bedrock and deterioration of the rock surface. A moment rigid connection requires grouting of the drilling hole.

Piles extended into the bedrock should be drilled at least 500 mm into it, irrespective of the working principle of the wall. It is recommended that piles transmitting vertical loads and piles whose lower ends are subject to significant moment loads and/or shear forces should have an
Table 7. Sectional properties and bending moment resistances of RD pile walls excluding corrosion allowance.

<table>
<thead>
<tr>
<th>RD pile wall</th>
<th>Pile</th>
<th>Sectional properties and bending moment resistances of RD pile walls, with 0.0 mm corrosion allowance</th>
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</thead>
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<tr>
<td></td>
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<td>12.5</td>
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*) The weight of pile pipe includes also the weight of the RM/RF interlocks.
Table 8. Sectional properties and bending moment resistances of RD pile walls with 1.2 mm corrosion allowance.

<table>
<thead>
<tr>
<th>RD pile wall</th>
<th>Pile</th>
<th>Sectional properties and bending moment resistances of RD pile walls, with 1.2 mm corrosion allowance</th>
<th>d [mm]</th>
<th>t [mm]</th>
<th>G [kg/m]</th>
<th>Weight [kg/m²]</th>
<th>b [mm]</th>
<th>W_b [cm⁴/m]</th>
<th>E</th>
<th>S355J2H M_{el} [kNm/m]</th>
<th>S440J2H M_{el} [kNm/m]</th>
<th>S460M H_{el} [kNm/m]</th>
<th>S550J2H H_{el} [kNm/m]</th>
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</thead>
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</table>

*) The weight of pile pipe includes also the weight of the RM/RF interlocks.
Table 9. Sectional properties and bending moment resistances of RD pile walls with 2.0 mm corrosion allowance.

<table>
<thead>
<tr>
<th>RD pile wall</th>
<th>Pile</th>
<th>Sectional properties and bending moment resistances of RD pile walls, with 2.0 mm corrosion allowance</th>
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</thead>
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<tr>
<td></td>
<td>1220.0</td>
<td>12.5</td>
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</tbody>
</table>

*) The weight of pile pipe includes also the weight of the RM/RF interlocks.
embedment length of at least 4 times the pile diameter. An RD pile wall bedrock contact can be assumed to be rigid if the embedment length of the piles is at least $4 \cdot d$ in the solid un-weathered bedrock, and by grouting the bore hole with grouting concrete C20/25. Deeper embedment length will not further increase the rigidity of the contact. However, a lower drilling depth quickly reduces pile rigidity, this also applies if the bore hole is not grouted.

Figure 14 shows the indicative maximum RD pile wall stiffness of $S_j$ (MNm/rad*m) for RD220/12.5... RD1200/12.5 walls using an embedment length of $4 \cdot d$ and C20/25 concrete grouting. In addition Figure 14 shows joint stiffness if the drilling depth is reduced to $3 \cdot d$. Joint stiffness is calculated for the bending moment equaling the elastic bending capacity of the pile pipe.

Figure 15 shows RD pile wall stiffness for non-grouted drilling holes. The applied bending moment was 0.5·elastic bending capacity of the pile pipe. The stiffness of the non-grouted RD pile wall was less than 3 % of a grouted wall in all cases.

The drill operator often interprets the bedrock as starting at the level where the pile first contacts the rock surface. However, the bedrock surface is in most cases uneven. It can be assumed that grouting of pile end is 100% successful after $1 \cdot d$ drilling. For these reasons, when estimating the rotational stiffness of the RD pile wall, the effective drilling depth is assumed to be somewhat shorter than the designed embedment length. With grouted piles the actual realized drilling depth is decreased by $2 \cdot d$ and with non-grouted by $1 \cdot d$.

**Figure 14. Stiffness of RD pile wall. Pile sizes RD220/12.5 ... 1200/12.5, RM/RF interlocks. Nominal strength of concrete grouting C20/25.**

<table>
<thead>
<tr>
<th>Pile Size</th>
<th>$S_j$ [MNm/rad*m]</th>
</tr>
</thead>
<tbody>
<tr>
<td>RD220/12.5</td>
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<tr>
<td>RD270/12.5</td>
<td>100</td>
</tr>
<tr>
<td>RD320/12.5</td>
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</tr>
<tr>
<td>RD400/12.5</td>
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</tr>
<tr>
<td>RD500/12.5</td>
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<td>600</td>
</tr>
<tr>
<td>RD1200/12.5</td>
<td>650</td>
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</table>

**Figure 15. Stiffness of non-grouted RD pile wall. Pile sizes RD220/12.5 ... 1200/12.5, RM/RF interlocks. Embedment length 3·d into integral bedrock.**

<table>
<thead>
<tr>
<th>Pile Size</th>
<th>$S_j$ [MNm/rad*m]</th>
</tr>
</thead>
<tbody>
<tr>
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<td>RD1000/12.5</td>
<td>24</td>
</tr>
<tr>
<td>RD1200/12.5</td>
<td>26</td>
</tr>
</tbody>
</table>
7.3 Interlock selection

The necessary angle changes in the RD pile wall line are effected by welding the interlocking sections at the desired angle. Figure 16. Interlocking section welded on opposite sides of a pile in line with each other allow only small angular deviations, at maximum ±5° from the straight wall line, Figure 17. Larger angular deviations must be implemented by welding interlocking sections at the desired angle.

Figure 16. Large angle change in RD pile wall line implemented by welding the interlock sections at the desired angle.

Figure 17. Small angle change in RD pile wall line implemented by the tolerances of the interlock sections.

Table 7 shows the theoretical run of the pile wall. The actual run of the wall, however, varies slightly due to pile deformation during installation, the out-of-roundness of pile pipes and the play of interlocking sections. The average width of a pair of jointed interlocking sections fitted with RM/RF interlocks is 64 mm and play about ±3 mm. According to standard EN 10219, the out-of-roundness tolerance of a structural pipe is ±2 % of its outside diameter. Subject to order, the out-of-roundness tolerance of spirally welded piles (≥ RD400) with interlocks may be smaller.

Table 10 shows the installation resistances of the interlock types used in SSAB RD pile walls. The given structural resistances are characteristic values determined from the full-scale laboratory tests according to EN 1990-1, Annex D.

An RD pile wall can be designed so that interlock sections transport long-term loads also in the completed structure. In long-term resistances, the effect of interlock corrosion must be taken into consideration. Table 11 gives the relative resistance reductions of RM/RF interlocks with various corrosion allowances (Table 10). Corrosion reduction is made from all soil-facing surfaces of the interlock sections excluding the contact surface between the male- and female sections.

Table 11. Relative capacity reductions of RM/RF-interlocks in long-term loadings due to corrosion.
7.4 Water tightness and groundwater management

The water tightness of an RD pile wall can be sufficient in some conditions without any special measures. The water tightness of the wall is greatly affected by the soil properties. In low water permeable soils (fine-grained soils) and moderate differential water pressure across the wall (< 50...80 kPa), the amount of water penetrating the interlock is negligible. With increasing differential water pressure and highly water-permeable soils, the probability of leaks through the interlock increases. Due to the installation method, no significant stresses are exerted on the interlocking sections during installation and no leakage points form in them due to deformations of the sections.

The water tightness of an RD pile wall can be improved by applying bitumen based sealing agent applied hot on the RF interlocking section either at the factory or on the site, or by using sealing compound that expands on contact with water, Figure 18a. When using a bitumen based sealant, the excess material is peeled out of the lock during the installation but it has no effect on the final water tightness. When working under cold conditions, the bitumen can be heated for example with propane torch prior to the pile installation to match the normal operating temperature. Excessive heating of the bitumen needs to be avoided, it breaks the structure of elastomers in bitumen. Water tightness can also be improved by grouting the area of the interlock behind the wall, Figure 18b. The results of water tightness tests of RM/RF interlocks with different sealing agents are given in section 6.4.

If water leaking through the interlocking section prevents the section from being closed by welding, a flat bar can be welded in front of the interlock and if necessary it and the area between the interlocking sections can be grouted, Figure 18d.

When an RD pile wall is subject to clear water tightness requirements, for example, when installing the RD pile wall is installed in water or below the groundwater table, it is always recommended to use some sealing agent in the interlocks. In these cases, strong water leakage usually prevents the sealing measured by welding. Sealing agents that are not water tight during installation (for example, some urethane based agents) are not suitable for situations where strong internal water flow is expected, such as earth dam improvements.

The water tightness of the lower end of the RD pile wall greatly depends on the groundwater conditions and water permeability of the bedrock and the soil layer directly above it. With conventional sheet pile walls, it is often difficult to achieve sufficient water tightness of the lower end of the wall without a concrete beam and/or grouting the soil and bedrock, because the retaining wall cannot be extended to follow tightly the bedrock surface which allows the flow across the surface under the wall.

When the piles of RD pile wall are extended into the bedrock, they block the direct flow route of water through the lower end of the wall, which considerably reduces, or maybe completely prevents, the filtration of water into the area inside the wall. The depth of drilling to bedrock and the depth of the pile toes in relation to each other is of great importance. For larger pile dimensions (D≥500) it is recommended to have a minimum drill depth of 1.5 m to solid bedrock. For smaller dimensions (D<500), it is recommended to have a minimum drill depth of 1 m to solid bedrock. It helps to achieve better watertightness, if adjacent piles can be extended as close as possible to same depth and if the interlocks in piles can be extended as close as possible to the lower end of the pile. When the RD pile wall extends to the bedrock, the water tightness of its lower end can be ensured, if necessary, by grouting the space between the piles and the bedrock.

If excavation is extended into the rock surface using an RD pile wall, it is possible to insert a concrete beam at the interface between the wall and the bedrock. If necessary, ground water flow across the bedrock can be prevented by sealing the bedrock under the retaining wall by grouting it through the pipe piles. If the lower ends of the pile piles in the RD pile wall are open, they may be used as pump wells to lower the ground water table.
Back of wall drainage

In some situations, for example in harbor quay walls, there might be a need for limiting the water level behind the wall. If in such cases the drainage needs to be done through the wall, maximum diameter of 60 mm weep holes can be done through the RM/RF interlocks.

Grouting

The injection channel of an RF lock section can be used to inject the lower end of the RD pile wall. It allows grouting the area underneath the lower ends of the interlocks. Figure 20a shows the principles of grouting.

If grouting is planned to be done through the injection channel in RF interlock, it is recommended to equip the channel with grouting connector at the top, blocking at the bottom and grouting valves. Grouting is done after the drilling and internal concreting of the piles. Grouting hose is connected to previously mentioned grouting connector with G1/2" threads. Flushing with water is not usually necessary. Grout will fill the voids of drill cuttings in the annulus, and the drill cuttings will work like aggregate in concrete. If valves have got blocked during drilling, water can be used to raise the pressure to open them. Also in these circumstances the pumping of water is stopped after the valves have opened. Usually valves will open with 2 – 3 bar pressure. Although in selection of grouting pump and hoses there is a need to prepare for clearly higher pressures due to possible blocking of the valves. Grouting is done with mixture of water and cement, where recommended water/cement ratio is 0.5. Suitable cement to be used in grouting is for example rapid cement, CEM II/A-LL 42.5 R.

During grouting the mass will flow in annulus also parallel to the RD pile wall. When the grouting mass hardens, this may cause blocking of some grouting valves. Therefore grouting needs to be tried from all the piles, even it might be impossible due to hardened grout. Recommended amount of grout is three times the theoretical volume of the annulus. The possible blocking of some valves can be covered with this excess grout material.

Grouting can also be performed from inside of the pile with the help of pile closing sleeve. The pile must not be able to rise due to the applied grouting pressure. If necessary, the pile can be rammed down again immediately after grouting. This is especially important with walls having significant vertical loads.

Different types of post-grouting can also be used on the unexcavated side of the RD pile wall to improve water tightness of the structure or to compact or reinforce the soil behind the wall. Grouting the background of an RD pile wall can be done by drilling or driving grout pipes behind the wall or to the joints of piles after the wall piles have been installed, Figure 20b. If necessary, grout pipes can also be attached to pile pipes before pile installation.

Water tightness of the section below excavation level can also be improved by grouting on the excavation side of the RD pile wall below the excavation level. The bedrock below the wall can be grouted through the piles of the RD pile wall. Grouting can be performed using e.g. cement- or bentonite-based grout.
### 7.5 Other structural components

An RD pile wall may be supported internally by bracing if the opposite RD pile wall or other structure providing support is sufficiently close. In permanent, for example, a ground/base slab, the intermediate floors of a building or the deck structure of a trough may act as horizontal braces.

Walings and clamps are implemented using steel beams. The distance between the support levels is determined according to the acting earth pressure and the stiffness of the applied retaining wall.

With internally supported walls, there are several details to be considered during design and dimensioning of the bracing, such as deflection of the compression struts due to dead load, accidental blows to the bracing system by machinery during excavation work, the concentration of loads centrally on struts in bracing joints, phasing and scheduling the excavation work and deformations of non-pretensioned supports during loading.

An RD pile wall can be supported externally by soil or rock anchors, or by tension rods attached to anchor plates as with other retaining wall structures. If external support is needed, anchors can be installed through the interlocking part of RD pile wall if the diameter of the hole is less than 60 mm with the RM/RF interlocks. If the support level can be located at the upper end of the RD pile wall, it is possible to make a separate console structure to avoid making holes for the anchors in the piles.
An RD pile wall can be fitted with various lining structures as necessary. Internal thermal insulation can be implemented, for instance, using polyurethane foam. Structures that need not be completely watertight can be lined, for instance, by shotcrete accompanied by installation of vertical drainage systems at the interlocking sections.

If the RD pile wall is used as a bearing structure that may take a fire load, such as in underground parking facilities, fire protection rules and regulations must be followed in the design and implementation of such a structure.

When determining the time-temperature dependency in fire design, it is recommended to use fire simulations based on the actual fire load. The standard fire exposure overestimates the thermal stress caused by the temperature increase. When determining the structural capacity of RD pile wall, it should be remembered that only half of the structure is exposed to the fire.

If the unprotected RD pile wall does not have the required structural integrity in fire, the wall can be designed as a concrete-filled composite structure with or without reinforcement, which usually ensures adequate fire resistance. If this is not possible or more fire protection is needed, the wall can be sprayed with fire-retardant. Dimensioning of these fire retardant materials must be based on studied and approved material properties.
7.6 Working order

As a rule, the implementation of installation and the installation sequence ought to be considered already at the wall design phase so as to minimize the number of wall ends that need to be joined to each other.

Both wall tolerances and installation tolerances must be considered in design. In the design and implementation of wall lines tolerances must be taken into account especially if the wall incorporates frame columns.

Due to the longitudinal tolerances of the wall, implementation of a closed wall, i.e. a wall where the last pile is joined by an interlock to the starting pile, is difficult. The exact pile spacing of a closed wall is not known before the other installation phases have been completed.

The wall ends can be joined by overlapping the end piles as shown in Figure 23. Piles of smaller diameter are used in the overlapping. The number of overlapped piles may be one or more, and the piles can be welded together at the point of overlap. Wall ends may also be overlapped using a pile that has no interlock but has a normal size ring pit as shown in Figure 24. The pile is placed on the unexcavated side of the wall and is supported by installed wall piles.

Ensuring adequate water tightness of overlapping solutions may require grouting of the soil around joints. It is recommended to take into account the end joints and the RD piles required for them already during the RD pile wall design phase.

An RD pile wall can be joined to a sheet pile wall if the interlocking sections of the latter match those of the RD pile wall. If the interlocking sections of the walls to be joined are different, a joint profile must be used to connect the interlocks of different types. If an RD pile wall is extended by a sheet pile wall, a narrow interlocking section E21 is attached to the RD pile as shown in Figure 25. If a sheet pile wall is extended by an RD pile wall, a wide interlocking section E21 is used as shown in Figure 26.

Figure 23. Joining wall ends by overlapping

![Figure 23. Joining wall ends by overlapping](image)

Figure 24. Joining wall ends by a loose pile.

![Figure 24. Joining wall ends by a loose pile.](image)

Figure 25. Narrow E21 interlocking section in RD pile wall - sheet pile wall connection.

![Figure 25. Narrow E21 interlocking section in RD pile wall - sheet pile wall connection.](image)

Figure 26. Wide E21 interlocking section in a sheet pile wall - RD pile wall connection.

![Figure 26. Wide E21 interlocking section in a sheet pile wall - RD pile wall connection.](image)
7.7 Special aspects to consider in design

Soil displacement

Soil displacement near RD pile walls is affected most by soil properties, but also by the drilling system, the implementation of the drilling work and the interlock type. RD pile walls are installed using oversized ring bits so as to leave a theoretically empty space outside the piles. The size of the empty space depends on the pile size and interlock type used.

In compact frictional soils, only minor soil displacement occurs near the RD pile wall. If compressed air flushing is used in the drilling, the empty space caused by the oversized ring bit is filled partly or entirely by drill cuttings. If the aim is to minimize displacement, compressed air and percussion force should be used only to the extent that flushing works and drilling progresses at a suitable rate.

In loose frictional ground, landfill and soft cohesive soil, settlement may take place in the immediate vicinity of the wall. Settlement may be caused by filling the empty space with the subsoil next to the wall. It may also be due to compressed air escaping outside the pile and resulting in loosening and disturbing the soil layers. Noticeable settlement may occur within half the pile length of the wall line. The extent of settlement greatly depends on the soil.

To minimize settlement, it is recommended to use a drilling system that allows the least amount of compressed air to escape into the soil around the pile.

Settlement of soft cohesive soils can be avoided by a technique where soil strata are penetrated by pressing or vibrating the open pipe pile with a variable frequency vibrator to the bottom of the soft soil strata. Thereafter, pile installation is continued by drilling. This technique requires the use of a so-called integrated ring bit.

When installing a micropile wall (RD220–RD320) a water-powered hammer with so-called external flushing can be used. This causes the empty space to be filled by drill cuttings and keeps soil deformations small.

On sites sensitive to soil settlement and displacement, where special attention is to be paid to settlement management, it is recommended to start the work by performing tests away from the structures to be heeded or to perform a pilot installation before actual installation to be able to reliably assess soil settlements.

Corners

Pile placement at the corners of an RD pile wall must be addressed during the design phase to ensure interlock sections attached to the piles can be welded at the correct angles. Figure 27 shows alternative solutions for normal RD pile wall corners. Methods for making corners and angular changes in RD pile wall are dealt also in chapter 7.3.

8 PRODUCTION OF RETAINING WALL STRUCTURES

General requirements concerning drilling equipment are given in Design and Installation Manual for RR and RD piles.

8.1 General

An RD pile wall is installed by the centric drilling method using ring bits of a larger diameter than standard bits. The ring bit drills a hole larger than the pile to accommodate the pile’s interlocks. Table 3 shows the recommended ring bit diameters for different piles and interlocking sections. In soft soil conditions where there are no stones or friction soil layers in ground, smaller diameter drill bits can also be used.
If the RD pile wall must also bear vertical loads, it is recommended the ring bit / casing shoe is at the bottom of the drilled hole. The ring bit / casing shoe must not be supported by the rock shelf unless the pile is filled with concrete or grout.

When using multi-wing pilot bits, the rockiness of the soil and sufficiently powerful drilling equipment must be taken into account. Penetration through rocky soil and boulders might occasionally be difficult and slow with multi-wing pilot bits. When leaving the piles of an RD pile wall in a moraine stratum, the stones in the soil may prevent the bit wings from closing and the drill bit from being lifted. Attention must also be given to ensuring sufficient rotation speed when drilling with multi-wing pilot bit.

Especially when using wing bits, but also when using ring bits, the compatibility of the tolerances of the pilot bit, the casing shoe and the pile pipe must be paid attention to. Particularly should be checked, if the tolerance between the head of the pilot bit and the casing shoe are suitable for the out of roundness tolerance of the pile pipe size in question.

As an alternative installation method, vibration or a combination of vibration and drilling can also be used. In this case, attention should be paid to the removal of possible obstacles on the surface, which will help to install an accurate wall.

### 8.2 Site preparation

The site must be prepared to ensure work can be done safely and efficiently.

Due to the height of the piling mast and long pile pipe, the drill rig has a high center of gravity. Good load-bearing capacity and flatness of the working platform are essential for safety at work. The working platform must be designed and dimensioned at the planning stage. If obstacles disrupting drilling are removed from the RD pile wall location, excavations need to be filled and compacted carefully. The working platform must not subside during drilling.

The level at which pile drilling is initiated must not be below the caterpillar level of the drilling rig. Drilling from lower level than the caterpillar level (drilling to trench) is unstable and inaccurate. It can also reduce working platform stability causing it to collapse and the drilling rig to fall over.

### 8.3 Storage and handling of pile pipes

Pile pipes must be stored and handled with care on site to prevent any significant damage to pile pipe straightness, interlock profiles and coatings. The storage and handling of piles on site are covered by a separate manual: “Piles and pile accessories, recommendations for safe handling for the customer”.

Piles and their accessories must be inspected immediately after delivery to the site. A visual inspection is made to ensure the shipment corresponds to the order and consignment note. The steel grade and dimensions of piles are verified from product descriptions and markings on the pile pipes. Pile sections and accessories must correspond to the products specified in the designs. A faulty or wrong product must not be installed.

Piles and their accessories must be inspected once more before installation. Pre-installation inspection ensures that the piles have not been damaged during handling and storage on site.

Pile sections and pile pipes are usually erected by a lifting cable or similar attached to near the head of the pile. Special care must be taken during erection to ensure, for example, that the lifting equipment / chain remains attached to the pile. It is recommended that in pile erection the piling equipment positioned at the pile during erection so that it does not need to be moved except for minor adjustment when the pile stands upright in the piling equipment.

Stress from curvature caused by the deadweight of a steel pile is never a critical factor when lifting RD micropiles. With large diameter piles ($d\geq 400$), the length limit for piles that can be lifted from the head without closer analysis is 20 meters. The erection of longer piles must be planned case by case, taking into account the pile dimensions. Piling rig stability must be considered in erection, and the weight and reach limitations and instructions for the rig must be taken into account in lifting.

### 8.4 Welding and cutting of steel elements

RD piles with interlocks can be spliced by welding if the required pile length exceeds the standard length pile that can be installed using the available pile drilling equipment. Splicing is done as normally with RD piles. The piles intended to be spliced are to be specified already when placing the order so that they can matched and marked as pairs. This makes splicing of piles on site much easier.

Splice welding of pile pipe with interlocks on site conditions requires special attention. It must be ensured that no angle change occurs between pile elements. A piece of interlock profile can help to get correct alignment for the interlocks. If necessary, bevels can be cut to the interlocks on site so that the pile pipe can be reliably welded also at the locations of the interlocks. Design and installation manual for RR and RD piles gives more information on requirements and also instructions on welding of RD piles. Appendix 5 of the manual has info on required preheat and hold times before commencing NDT.

When the RD pile has reached its target level, the pile section remaining above ground can be cut off. The need to cut depends on the used drilling equipment. If the next pile can be installed in interlock of the previous one that may extend quite high above ground level, there is no need to cut the previous pile to facilitate the work. The final cutting of piles is done perpendicularly at the cut-off height according to plan. Piles may be cut, for instance, by a flame cutter or a plasma cutter.

The rules of procedure must be paid particular attention when cutting RD piles in special situations when the part to be removed can not be normally lifted / fell directly
away (for example if piling rig and drill pipes are still attached to pile while the pile is cut). In such case the part which will be removed must be "peeled open". Due to the manufacturing methods of pile pipes, there might be stresses left in them. Therefore cutting of pile by "peeling" must be made in sequences shown in Figure 16. Longitudinal cut, for the whole length of the part to be removed, must be made first. After the longitudinal cut has been made, the pile can be cut normally from the design cut-off elevation. Cutting must be started from the point where longitudinal cut has ended.

Figure 28. Cutting an RD pile by “peeling”

8.5 Drilling of pile pipes

Installation of an RD pile wall places no special demands on the features of the installation equipment, which means that normal pile drilling equipment can generally be used. However, it must be ensured that jaws and other parts of the equipment can accommodate the interlocking sections welded to the sides of the piles. It is recommended to have such supports in jaws of drill rig, where the interlock profile can be supported in two directions during installation of the piles. At the direction of the wall line the support helps during positioning of the pile and during beginning of the drilling, placing the RF interlock profile to correct position when connecting to RM interlock profile. In transverse direction to the wall line the support prevents the pile from rotating during installation. It is important to guide the pile pipe with jaws to ensure the RD pile wall is straight. Use of the longest possible pile sections to minimize splice welds facilitates pile wall installation.

If highly accurate alignment is required, it is recommended that the piles are installed through a guide frame built at ground level. Guide frame is installed while making piling platform.

To ensure drilling accuracy and stability during the drilling of RD piles and the RD pile wall, the base of the piling mast must be supported firmly to caterpillar track level and the DTH hammer with drill tubes must be eccentric to pile pipe. An unstable drilling position can cause inaccurate pile locations, interlock jamming and tearing, or casing shoe detachment if the longitudinal axis of the piles does not remain parallel.

First pile

Installation of an RD pile wall is usually started at the point where the bedrock surface is deepest. The next pile can be drilled deeper than the previous one, but this must be taken into account in the length of the RF interlock. The next pile can be drilled only as much deeper as the RF interlock is missing from pile end, as shown in Figure 29.

During installation of the first pile, it must be ensured that the interlocks stay aligned as planned and the pile pipe does not rotate. The best way to ensure the position of first pile and the direction of the interlocks is to support the interlocks in the jaws of the drilling rig. Special attention must be paid to inclination of the first pile to ensure wall straightness. Pile inclination must be taken into account also when installing subsequent piles. If a pile is askew, this can damage the interlocks or it may try to “fall” the wall. The next pile always supports the previous pile which keeps them better aligned. Where the line of wall needs to be especially accurate, use of a guide frame is recommended.

The first pile of an RD pile wall must not have an RF interlock, see Figures 11 and 12. The drill bit makes a hole where only an RM interlock can fit. If installation continues in both directions from the first pile, two RM interlocks must be attached to the first pile.

Subsequent piles

An RD pile wall can be installed either in the direction of the wall line by backing up the drilling rig, or from the side, depending on the equipment used. The wall can be installed from either side or in either direction. However, installation is always done so that an RM interlock is on the side of direction of installation. Installation may also begin from the middle of the wall line or from a corner using a pile onto which two similar RM interlocks have been attached.

When an RD pile encounters a large stone, boulder or bedrock, the pull down force is kept low and rotation speed is increased. This reduces the tendency of the pile to change direction during drilling. It also ensures a reliable installation process as stresses on the interlocking sections and friction remain low.

On a sloping bedrock surface, it is advisable to install the piles of an RD pile wall in the direction of upward sloping bedrock so that the interlocking sections can be extended close to the tip of the pile pipe. If it is assumed that the bedrock surface declines in the direction of installation, and a pile has to be drilled deeper than the previous one, the RF interlock must not extend to the tip of the pile, see Figure 29. If a RF interlock extends to the tip of a pile, it will collide with the ring bit of the previous pile or with the bedrock preventing installation at a lower level than the previous pile. In the case of pile walls whose lower section is subject to water tightness requirements, the interlocking sections must extend as low as possible.

For instance, if it is desired to install a pile 3 metres deeper than the previous one, the RF interlock must end at least 3 meters before the pile end. Figure 29. Since that requires installing the pile for the first 3 meters without the pile being joined to the previous one by an interlocking
Section 8.6 Tolerances regarding plan position and verticality

Inaccuracy of an RD pile wall is usually small due to the drilling method. Stones and boulders in ground do not usually cause inaccuracy the positioning of an RD pile wall. If necessary, RD pile wall accuracy can be improved by using a guide frame during installation.

Inclination of an RD pile wall needs extra attention if the wall forms a closed structure or if some other things impose stricter tolerances on wall inclination.

If the RD pile wall is not joined at its ends to other structures or if perpendicularity is not otherwise important, the tolerances are similar to drilled piles.

Unless otherwise stated in design, the measurement accuracy of the location of pile pipes before and after installation is 10 millimeters. Figure 30 shows the definitions for tolerances used in construction.
Tolerances can be agreed separately before installation if structural demands, soil conditions or drilling equipment used imposes stricter tolerances or allows larger tolerances than those given here. Table 12 shows the tolerances allowed for RD pile walls.

**Table 12. Tolerances allowed for RD pile walls**

<table>
<thead>
<tr>
<th>Type of RD pile wall</th>
<th>Plane position of pile top</th>
<th>Inclination tolerance upright piles or inclined piles with inclination of $n \geq 15 \left( \Theta \geq 86^\circ \right)$</th>
<th>Inclination tolerance inclined piles with inclination of $4 \leq n &lt; 15 \left( 76^\circ \leq \Theta &lt; 86^\circ \right)$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Temporary structure, no vertical loads</td>
<td>$\leq 50$ mm</td>
<td>$\leq 2% \left( 0.02 \text{ m/m} \right)$</td>
<td>$\leq 4% \left( 0.04 \text{ m/m} \right)$</td>
</tr>
<tr>
<td>Permanent structure or vertical loads</td>
<td>$\leq 25$ mm</td>
<td>$\leq 1.5% \left( 0.015 \text{ m/m} \right)$</td>
<td>$\leq 2.5% \left( 0.025 \text{ m/m} \right)$</td>
</tr>
</tbody>
</table>

**8.7 Pile pipe position correction during driving**

Drilling as an installation method and the stiffness of RD pile pipes reduce the tendency to incline forward during installation. However, inclination may occur while using large, powerful drilling rigs. Inclination can be reduced by using a guide frame of sufficient stiffness and stability, and by reducing pull down speed. These methods ensure reliable installation with low stresses and friction to interlock sections.

**8.8 Installation of anchorages**

An RD pile wall can be supported externally by soil or rock anchors, or by tension rods attached to anchor plates in the same way as other retaining wall structures. The hole needed for the anchor is drilled, for example, with diamond drilling. Efforts are primarily made to drill an anchor hole in the center of the pile, but if necessary, a hole can also be drilled at the interlock. In demanding conditions, soil and water leakage through the hole requires special attention, for example, when the hole is under the groundwater table or when soil granularity is very fine. Fast curing concrete or a separate collar around the anchor casing can be used to control leaking soil and water. Measures needed after anchor stress must be considered when using fast curing concrete. When making a watertight RD pile wall, also water tightness of the connection between the anchor casing and bedrock must be taken into account.

**8.9 Walings and compression struts**

Walings and compression struts are made from steel. Hollow sections or HEB-profiles can be used.

Detailed designs and drawings are needed from all joints between the walings and struts. All splices must be located as shown in the drawings.

Loads must be centralized on compression struts. This is why special attention needs to be paid to cutting the heads of compression struts and for joints between compression struts and walings.

All supporting structures need to be firmly joined to the RD pile wall to ensure they do not detach due to contacts from machinery or wall movement.

**8.10 Excavation, filling, drainage and de-watering**

Excavation is made in accordance with the excavation plan, each support level at a time. Sufficient safety must be in place during excavation work to ensure the sloping edge of the excavation pit does not collapse. While excavating below working level, the weight of the excavator and any working platform load the edge.

Construction work in excavation is usually done in dry conditions, in which case the bottom of the excavation should be kept dry. As minimum, the excavation pit should have rainwater and meltwater drainage.

When lowering groundwater in an excavation pit, groundwater lowering and excavation stages must be coordinated with each other. Groundwater lowering must be verified from observation wells in the excavation area.

**8.11 Extraction of pile pipes**

The piles of an RD pile wall installed in temporary structures may be reused several times. If necessary, RD piles are to be filled with soil before extracting them so as to avoid major settlements or hazards. After the extraction of a temporary RD pile wall, the underlying subsoil and possible structural layers must be compacted to the density required by the site.

Extraction may be done, for instance, by a vibratory hammer. The impact of any integrated ring bit on pile extraction should be considered in the case of RD pile walls to be extracted.

**8.12 Rock dowels and anchor bolts**

The lower end of an RD pile wall can be supported on the bedrock by drilling all or some of the piles into it. The lower end can also be supported on bedrock by drilling separate anchors, rock dowels or smaller drilled piles through the pile pipes into the bedrock. When the piles are installed in the bedrock, a concrete beam at the lower end of the RD wall is not normally needed to support the lower end of the wall. If the RD pile wall is not extended into the
bedrock, it is supported by passive earth pressure in the same way as a conventional retaining wall structure.

Owing to the high bending stiffness of the RD pile wall, the distance between the support levels can be made longer compared, for instance, to a sheet pile wall. By extending the RD pile wall sufficiently into the bedrock and by grouting behind the interlocking sections, if necessary, the retaining wall can be made to act partly as a mast structure of high bending moment stiffness, which reduces the need for support levels. The RD pile wall can be supported by internal or external supports.

8.13 Sealing

Water tightness of the interlocks used in RD pile walls can be improved using the methods described in sections 6.4 and 7.4. The final level of water tightness depends on the sealant material and method used, installation work, soil conditions and the hydrostatic pressure on different sides.

Besides sealing the interlocks, the soil behind an RD pile wall can be grouted to make it watertight as shown in section 7.4. Grouting can be done through a grout channel in the interlock or by using a separate grout channel.

Grouting can be done for the whole length of the pile by perforating the grouting channel in the RF interlock. Based on test grouting, the maximum distance between holes is 1 meter and distance from uppermost hole to ground level is about 2 meters. The amount of grout used must be clearly bigger than theoretical amount needed; based on tests it should be at least three times bigger. Grout will flow first to those areas with easy access. When those areas have filled, the grout will flow to other areas. To avoid the grout channel filling with soil during drilling, the grout holes must be plugged.

Grouting between the bedrock and RD pile wall is inspected visually when excavation reaches the bedrock surface. If necessary, tightness can be improved by soil grouting, concrete beam, jet grouting or bedrock curtain grouting.

8.14 Surface treatments and linings

An RD pile wall can be delivered with coating as described in section 7.5. Possible damage to the coating depends greatly on the installation work and soil conditions.

When an RD pile wall is coated on site after installation, it can be coated with several different paints or masses as needed. The pile surface must be cleaned as required by the coating employed.

An RD pile wall can also be covered with different panels or casettes. Lining can be attached either directly to piles or to a separate frame. When using a separate frame, possible deviations in the RD pile wall can be straightened.

9 SUPERVISION, TESTING AND MONITORING

In its operations, SSAB follows procedures that comply with the requirements of the ISO 9001:2008 quality management system and the ISO 14001:2004 environmental management system. Quality management systems ensure the functioning of processes from raw materials procurement to delivery of the end product to the customer.

SSAB steel pipe piles are made of high-quality steel produced at the company’s steel mill in Raaha. Large diameter (≥RD400) steel pipe piles are manufactured by spiral joint welding and small diameter piles (≤RD320) by longitudinal welding. Interlocking sections are welded simultaneously to both sides of the spirally welded RD piles on an automated production line. Special attention has been paid to control of deformations of steel pipes due to welding the interlocking sections.

The steel piles used in SSAB’s RD pile wall are CE-marked products and have been granted European technical approval ETA 12/0526.

Technical delivery conditions

The technical delivery conditions of piles comply with standard EN 10219-1. Dimensions and tolerances comply with standard EN 10219-2. A material certificate in accordance with EN 10204 type 3.1 for the pile material is provided.

9.1 Supervision

Supervision of the all work related to a retaining wall structure must be done at least according to Chapter 4 of EN 1997-1. In addition, piling work is supervised according Chapter 7 of EN 1997-1. Supervision of the construction process, including workmanship, and any monitoring of the performance of the structure during and after construction, must be specified in the Geotechnical Design Report.

The plan should specify the type, quality and frequency of supervision, which should be commensurate with the:
- degree of uncertainty in the design assumptions
- complexity of the ground and loading conditions
- potential risk of failure during construction
- feasibility of implementing design modifications or corrective measures during construction.

In addition, the plan included in the Geotechnical Design Report must state acceptable limits for the results to be obtained by supervision.

Construction work must be inspected on a continuous basis and the inspection results must be recorded.
Records shall be maintained of at least the following:
• sequence of inspections
• content of each inspection
• critical values of transformations, forces and water levels

9.2 Testing

Ground condition testing must be done according to Chapter 3 of EN 1997-1.

Possible pile load tests for the RD pile and the RD pile wall primary and secondary elements must be carried out according to Chapter 7.5 of EN 1997-1.

9.3 Monitoring

Different phases of RD pile wall installation must be monitored. The monitoring program must be carried out in accordance with the Geotechnical Design Report. Process description and implementation plan must be according to EN 1997-1.

If project is located in a built-up area, the ground vibrations and noise levels arising from construction work must be followed up and registered regularly. In addition, the impact of piling on any nearby easily damaged buildings or unstable slopes must be observed. Observation methods can be, for instance, measurement of vibrations, capillary water pressure, and transformation or tilt. Measurement performed according to local practice to ensure the results can be compared to the criteria for the area.

Observation frequency must be defined and agreed before starting piling work. Measurement records must be prepared at agreed intervals and be available at the site until piling has been completed, after which they will be archived.

All equipment used for follow-up and monitoring must be appropriate and calibrated.

All deviations to the plans arising whilst work is being carried out must be reported and documented.

An experienced drill operator can estimate how solid the rock is by observations made during drilling and the settlement speed of the pile pipe. Based on these observations, the responsible foundation engineer can estimate the sufficiency of the geotechnical resistance. If needed, geotechnical resistance can be measured by a static or dynamic load test.

Displacements of already installed piles must be followed continuously during installation work. After piling work has been completed, pile location displacements must be measured at cut-off level. If displacement is larger than allowed in the plans, the responsible foundation engineer will analyze how this excess affects stresses arising in the piles and superstructures. The decision as to whether or not these piles can still be accepted is made based on this analysis.

The completed structure will be documented after piling. Documentation must include the pile locations and dimensions and the level of the upper and lower heads of the piles. Measurement must take place as soon as possible after installation. The accuracy for location is 10 mm, for level 5 mm, for inclination 0.5 % and for direction 5 gon.

Verification reports of the piles and any other construction documents shall be archived as required by contracts and statutory requirements.

Pile straightness must be inspected and documented after installation. For the piles that are empty and dry after installation, inspection is usually made by lowering a torch with measuring tape into the pile pipe. The straightness of pile can be estimated based on depth when the light disappears. More precise measurement can be made, for instance, with an inclinometer where required. Piles failing to meet straightness criteria are reported to the responsible foundation engineer, who will then decide on any further action.

Where the level of ground-water or free streaming water is a critical parameter in design, the levels must be monitored and measured sufficiently frequently to provide a reliable impression. It is recommended that ground-water level or pore-water pressure continues to be monitored after installation until it is verified that there are no adverse impacts.

The horizontal deviation in the upper surface of retaining wall must be monitored regularly in predefined positions. Accuracy must be sufficient to compare the results to the designed values. When a retaining wall is located near easily-damaged buildings or sensitive equipment, the following points at least must also be considered:
• measuring displacement at a certain depth
• measuring the subsidence of these buildings
• measuring the anchoring forces.

10 CONSTRUCTION SITE DOCUMENTATION

All significant quality assurance measures must be documented. Inspection documents must be dated and signed. Documents must be filed in the construction site quality folder, which must be updated continuously. Once construction has been completed, the contractor must submit a copy of the quality folder to the developer.
10.1 Installation phase worksite documents

Worksite documents related to the supervision, testing and monitoring and measuring of permanent retain wall structures referred to in chapter 9 must be available at the construction site.

10.2 Final phase worksite documents

The final worksite documents must include following information:
- the actual locations of the retaining wall and the additional structures remaining in the ground in relation to the reference point or reference lines
- a list of significant information related to use, maintenance and inspection of the structure
- information about the groundwater level and pore-water pressure given in the design report
- special instructions concerning actions to be taken after installation has been completed where such action is deemed necessary due to observations made during installation
- maintenance instructions for drying systems, methods to be used and frequency of maintenance
- restrictions regarding additional loads behind the wall
- displacement during the construction of the retaining wall
- incidents adversely affecting installation and how the effects of these were dealt with
- record of any damage to nearby buildings
- results of penetration and loading tests.

11 SPECIAL REQUIREMENTS

Until such time as similar European standards are available, local national standards, instructions and definitions must be followed in matters concerning
- worksite safety
- safety of working methods
- legality of the manual working phases and inspections to be done during excavation
- reliability and safety of the piling equipment and other apparatus and tools used in piling and excavation work

11.1 Safety

Requirements of the safety regulations as well as European and national standards and quality criteria must be complied with in the manufacture of retaining wall structures.

Piling machinery and equipment must comply with standards EN 16228-1, -2 and -7 (2014).

Piling or excavation work must comply with safety aspects applying to:
- worksite safety
- operational safety of the pile driver and other equipment and tools used in piling
- safety of working methods.

Particular attention must be paid to:
- all work phases requiring working near heavy machinery and equipment, and heavy tools
- the danger related to open excavation pits / open pile pipes
- manual work phases and inspections to be performed inside RD pile wall excavation pits
- lifting and moving of piles and reinforcements.

Manual excavation work must be kept to minimum. It must also be limited to dry soil conditions, where the soil is naturally stable, and where the walls of the excavation pit are constantly supported.

Working is prohibited in trenches or excavation pits if the available space for piling is less than 0.75 meters in diameter.

11.2 Impact on surrounding buildings and installations

If there are structures and installations in the vicinity of the construction site which are vulnerable to constructional damage, the condition of these structures must be carefully established and documented before work begins.

Disruption and possible damage to the surroundings caused by piling work must be kept to a minimum and below the specified limit values.

Disruption and environmental nuisance may include
- shifting and / or compaction of the soil layer
- disturbance of the soil and increase of pore water pressure
- vibrations
- noise
- soil, water and air pollution.
The nature and extent of any disruption or environmental nuisance depends on the:
- location of the piling site
- soil and ground water conditions at the site
- piling method
- working order and work phase.

National discharge standards and other national standards concerning the protection of the surroundings must be complied with where no European standards are available. Suitability of the materials used in the environment concerned must be proved. This must be agreed with the customer, who confirms the use of materials and supplies.

11.3 Noise abatement

Special precautions shall be taken to ensure noise levels remain within the limits provided by international or national regulations.

If persons in the vicinity of the piling site are likely to be exposed to noise, the expected noise level must be estimated or demonstrated by comparable experience from similar sites or by test piling. Assessment of the acceptability of the piling work is done based on these estimations. If necessary, the noise level should be monitored during piling work to ensure the noise level remains within the agreed limits.

At worksites, where noise level exceeds 80 dB, hearing protection must be used.

Outsiders must be prevented from entering the noise impact area.

11.4 Permeability of retaining walls

The water tightness of an RD pile wall greatly depends on groundwater conditions and water permeability of the bedrock and the soil layer directly above it. When the piles of RD pile wall are extended into the bedrock, they block the direct flow route of water through the lower end of the wall. This considerably reduces, or perhaps completely prevents, the filtration of water into the area inside the wall. When the RD pile wall extends into the bedrock, the water tightness of its lower end can be ensured, if necessary, by grouting the space between the piles and bedrock.

Water tightness of an RD pile wall can be improved by applying a bitumen-based sealing agent, applied hot, on the RF interlock either in factory or on site or by using sealing compound that expands in contact with water, Figure 18a. Water tightness can also be improved by grouting the interlock area behind the wall, Figure 18b.

The best possible water tightness of the RD pile wall can be achieved by welding shut the space between interlocking section and the pipe pile after the excavation has been completed, Figure 18c.

If water leaking through the interlocking section prevents the section being closed by welding, a flat bar can be welded in front of the interlock, Figure 18d.

The water tightness of the lower end of the RD pile wall greatly depends on groundwater conditions and water permeability of the interlock area. When the piles of RD pile wall are extended into the bedrock, they block the direct flow route of water through the lower end of the wall. This considerably reduces, or perhaps completely prevents, the filtration of water into the area inside the wall. When the RD pile wall extends into the bedrock, the water tightness of its lower end can be ensured, if necessary, by grouting the space between the piles and bedrock.
Figure 31. Data included in RD pile wall design.

The pile situation plan for the RD pile wall must show:

- Piles with individual identifiers; code or colour
- Installation starting points
- Direction of installation
- Possible wall-end joints and details

Starting point
Direction of installation
Joint

Top view of pile

In deviation from the assumption:
RM interlock
No interlock

The pile situation plan for the RD pile wall must show:

- Piles with individual identifiers; code or colour
- Installation starting points
- Direction of installation
- Possible wall-end joints and details

Basic principle:

Pile identifier: 

Pile size: 

Wall thickness: 

Pile steel grade: S355J2H
S440J2H
S550J2H
X60
X70

Interlock type: RM/RF
E21

Splicing on site: yes
no

Necessary end bevels must be made known when placing order.

Pile accessories: Grouting pipes
Other accessories

A plan of all accessories must be presented.
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